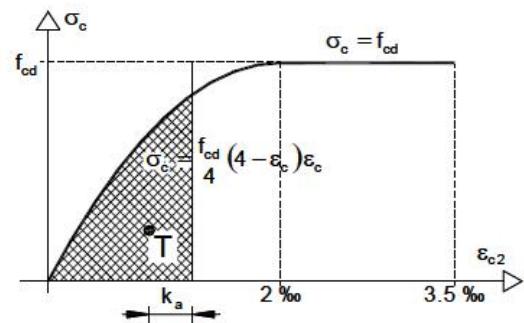
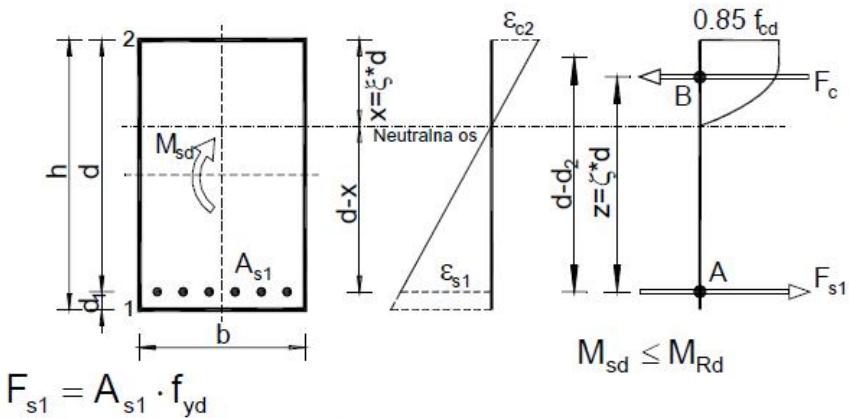


Djelovanje	Parcijalni koeficijenti sigurnosti γ_F		
	Vrsta djelovanja		
	Stalno γ_G	Promjenjivo γ_Q	Prednapinjanje γ_P
Nepovoljno	1.35	1.5	1.0 ili 1.1
Povoljno	1.0	0	1.0 ili 0.9

Vrsta kombinacije	Parcijalni koeficijenti sigurnosti γ_m	
	Beton γ_c	Betonski i prednapeti čelik γ_s
Osnovna kombinacija	1.50	1.15
Slučajna kombinacija	1.30	1.00

Dimenzioniranje na moment savijanja – osnovni izrazi



$$\alpha_v = \frac{\varepsilon_{c2}(6 - \varepsilon_{c2})}{12} \quad 0\% < \varepsilon_{c2} \leq 2\%$$

$$\alpha_v = \frac{3\varepsilon_{c2} - 2}{3\varepsilon_{c2}} \quad 2\% < \varepsilon_{c2} \leq 3.5\%$$

$$k_a = \frac{8 - \varepsilon_{c2}}{4(6 - \varepsilon_{c2})} \quad 0\% < \varepsilon_{c2} \leq 2\%$$

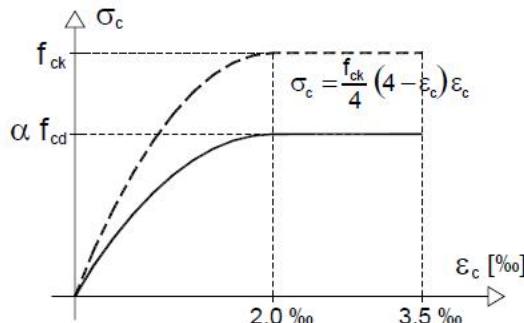
$$k_a = \frac{\varepsilon_{c2}(3\varepsilon_{c2} - 4) + 2}{2\varepsilon_{c2}(3\varepsilon_{c2} - 2)} \quad 2\% < \varepsilon_{c2} \leq 3.5\%$$

$$\sum N = 0 \Rightarrow F_c = F_{s1}$$

$$0.85 \cdot \alpha_v \cdot \xi \cdot d \cdot b \cdot f_{cd} = A_{s1} \cdot f_{yd}$$

$$\omega = 0.85 \cdot \alpha_v \cdot \xi = \frac{A_{s1}}{d \cdot b} \cdot \frac{f_{yd}}{f_{cd}} = \rho \cdot \frac{f_{yd}}{f_{cd}}$$

Karakteristika betona	C12/15	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60	
f_{ck} (MPa)	Čvrstoća na valjku	12	16	20	25	30	35	40	45	50
$f_{c,cub}$ (MPa)	Čvrstoća na kocki	15 (MB 15)	20 (MB 20)	25 (MB 25)	30 (MB 30)	37 (MB 40)	45 (MB 45)	50 (MB 50)	55 (MB 55)	60 (MB 60)
$f_{ct,m}$ (MPa)	Srednja vlačna čvrstoća	1.6	1.9	2.2	2.6	2.9	3.2	3.5	3.8	4.1
τ_{Rd} (MPa)	Posmična čvrstoća	0.18	0.22	0.26	0.30	0.34	0.37	0.41	0.44	0.48
E_{cm} (MPa)	Početni modul elastičnosti	26000	27500	29000	30500	32000	33500	35000	36000	37000



Koefficijentom "α" uzima se u obzir nepovoljno djelovanje dugotrajnog opterećenja i dinamičkih učinaka. Za "α" se uzima:

α = 0.85 za presjeke oblika pravokutnika

α = 0.80 za presjeke oblika trokuta ili trapeza

$$E_{cm} = 9500 \cdot \sqrt[3]{f_{ck} + 8} \quad [\text{MPa}] ; \quad f_{ck} \quad [\text{MPa}]$$

$$f_{ct,m} \approx 0.3 \cdot (f_{ck})^{2/3} \quad [\text{MPa}] ; \quad f_{ck} \quad [\text{MPa}]$$

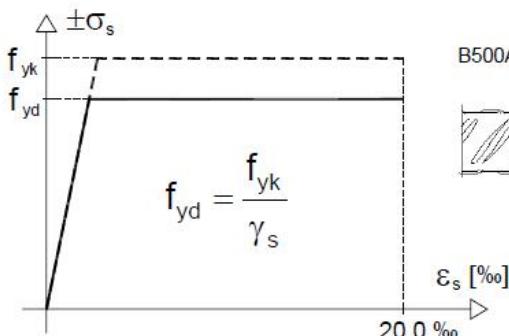
$$f_{cd} = \frac{f_{ck}}{\gamma_c}$$

Koefficijenti sigurnosti na materijal

Materijal	Beton (γ_c)	Čelik (γ_s)
Kombinacija		
Uobičajena kombinacija	1.50	1.15
Izvanredna kombinacija	1.30	1.00

Svojstva čelika za armiranje:

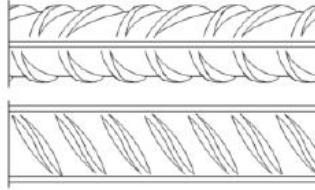
	Šipkasta armatura (nHRN EN 10080-2, nHRN EN 10080-3 i nHRN EN 10080-4)				Mrežasta armatura (nHRN EN 10080-5)		
Naziv i oznaka (broj) čelika	B500A (1.0438)	B500B (1.0439)	B450C (1.04...)	B500A (1.0438)	B500B (1.0439)	B450C (1.04...)	
Nazivni promjer, d (mm)	Namot: 4-16 Šipke: 6-40	Namot: 6-16 Šipke: 6-40	Namot: 6-16	5-16	6-16	6-16	
Granica razvlačenja f_{yk} (MPa)	≥ 500	≥ 500	≥ 450	≥ 500	≥ 500	≥ 450	
Omjer vlačne čvrstoće i granice razvlačenja	≥ 1.05	≥ 1.08	≥ 1.15 ≤ 1.35	≥ 1.05	≥ 1.08	≥ 1.15 ≤ 1.35	



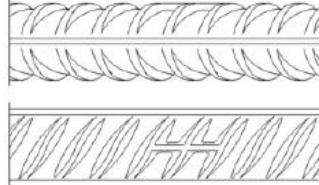
B500A – tri reda poprečnih rebara



B450C – dva reda poprečnih rebara; s jedne strane rebara pod različitim kutovima u odnosu na os



Materijal	Beton (γ_c)	Čelik (γ_s)
Kombinacija		
Uobičajena komb.	1.50	1.15
Izvanredna komb.	1.30	1.00



B500B – dva reda poprečnih rebara; s obje strane rebara su paralelna (pod istim kutom u odnosu na os)

Lom po betonu:					
e _{c2} %o	e _{s1} %o	x=x/d	z=z/d	w ₁ %	m _{sd}
3.50	20.00	0.149	0.938	0.103	0.096
3.50	19.75	0.151	0.937	0.104	0.097
3.50	19.50	0.152	0.937	0.105	0.098
3.50	19.25	0.154	0.936	0.106	0.099
3.50	19.00	0.156	0.935	0.107	0.100
3.50	18.75	0.157	0.935	0.108	0.101
3.50	18.50	0.159	0.934	0.110	0.102
3.50	18.25	0.161	0.933	0.111	0.103
3.50	18.00	0.163	0.932	0.112	0.104
3.50	17.75	0.165	0.931	0.113	0.106
3.50	17.50	0.167	0.931	0.115	0.107
3.50	17.25	0.169	0.930	0.116	0.108
3.50	17.00	0.171	0.929	0.118	0.109
3.50	16.75	0.173	0.928	0.119	0.110
3.50	16.50	0.175	0.927	0.120	0.112
3.50	16.25	0.177	0.926	0.122	0.113
3.50	16.00	0.179	0.925	0.124	0.114
3.50	15.75	0.182	0.924	0.125	0.116
3.50	15.50	0.184	0.923	0.127	0.117
3.50	15.25	0.187	0.922	0.129	0.119
3.50	15.00	0.189	0.921	0.130	0.120
3.50	14.75	0.192	0.920	0.132	0.122
3.50	14.50	0.194	0.919	0.134	0.123
3.50	14.25	0.197	0.918	0.136	0.125
3.50	14.00	0.200	0.917	0.138	0.126
3.50	13.75	0.203	0.916	0.140	0.128
3.50	13.50	0.206	0.914	0.142	0.130
3.50	13.25	0.209	0.913	0.144	0.131
3.50	13.00	0.212	0.912	0.146	0.133
3.50	12.75	0.215	0.910	0.148	0.135
3.50	12.50	0.219	0.909	0.151	0.137
3.50	12.25	0.222	0.908	0.153	0.139
3.50	12.00	0.226	0.906	0.155	0.141
3.50	11.75	0.230	0.905	0.158	0.143
3.50	11.50	0.233	0.903	0.161	0.145
3.50	11.25	0.237	0.901	0.163	0.147
3.50	11.00	0.241	0.900	0.166	0.150
3.50	10.75	0.246	0.898	0.169	0.152
3.50	10.50	0.250	0.896	0.172	0.154
3.50	10.25	0.255	0.894	0.175	0.157
3.50	10.00	0.259	0.892	0.179	0.159
3.50	9.75	0.264	0.890	0.182	0.162
3.50	9.50	0.269	0.888	0.185	0.165
3.50	9.25	0.275	0.886	0.189	0.167
3.50	9.00	0.280	0.884	0.193	0.170
3.50	8.75	0.286	0.881	0.197	0.173
3.50	8.50	0.292	0.879	0.201	0.176
3.50	8.25	0.298	0.876	0.205	0.180
3.50	8.00	0.304	0.873	0.210	0.183
3.50	7.75	0.311	0.871	0.214	0.186
3.50	7.50	0.318	0.868	0.219	0.190
3.50	7.25	0.326	0.865	0.224	0.194
3.50	7.00	0.333	0.861	0.230	0.198
3.50	6.75	0.341	0.858	0.235	0.202
3.50	6.50	0.350	0.854	0.241	0.206
3.50	6.25	0.359	0.851	0.247	0.210
3.50	6.00	0.368	0.847	0.254	0.215
3.50	5.75	0.378	0.843	0.261	0.220
3.50	5.50	0.389	0.838	0.268	0.224
3.50	5.25	0.400	0.834	0.275	0.230
3.50	5.00	0.412	0.829	0.284	0.235
3.50	4.75	0.424	0.824	0.292	0.241
3.50	4.277	0.450	0.813	0.310	0.252
3.50	4.25	0.452	0.812	0.311	0.253
3.50	4.25	0.452	0.812	0.311	0.253
3.50	4.00	0.467	0.806	0.321	0.259
3.50	3.75	0.483	0.799	0.332	0.266
3.50	3.50	0.500	0.792	0.344	0.273
3.50	3.25	0.519	0.784	0.357	0.280
3.50	3.00	0.538	0.776	0.371	0.288
3.50	2.75	0.560	0.767	0.386	0.296
3.50	2.50	0.583	0.757	0.402	0.304
3.50	2.25	0.609	0.747	0.419	0.313
3.50	2.00	0.636	0.735	0.438	0.322
3.50	1.75	0.667	0.723	0.459	0.332
3.50	1.50	0.700	0.709	0.482	0.342
3.50	1.25	0.737	0.693	0.507	0.352
3.50	1.00	0.778	0.676	0.536	0.362
3.50	0.75	0.824	0.657	0.567	0.373
3.50	0.50	0.875	0.636	0.602	0.383
3.50	0.25	0.933	0.612	0.643	0.393
3.50	0.00	1.000	0.584	0.689	0.402

Lom po armaturi:					
e _{c2} %o	e _{s1} %o	x=x/d	z=z/d	w ₁ %	m _{sd}
3.50	20.00	0.149	0.938	0.102	0.096
3.45	20.00	0.147	0.939	0.101	0.095
3.40	20.00	0.145	0.940	0.099	0.093
3.35	20.00	0.143	0.941	0.098	0.092
3.30	20.00	0.142	0.942	0.096	0.090
3.25	20.00	0.140	0.943	0.094	0.089
3.20	20.00	0.138	0.944	0.093	0.088
3.15	20.00	0.136	0.944	0.091	0.086
3.10	20.00	0.134	0.945	0.090	0.085
3.05	20.00	0.132	0.946	0.088	0.083
3.00	20.00	0.130	0.947	0.086	0.082
2.95	20.00	0.129	0.948	0.085	0.080
2.90	20.00	0.127	0.949	0.083	0.079
2.85	20.00	0.125	0.950	0.081	0.077
2.80	20.00	0.123	0.951	0.080	0.076
2.75	20.00	0.121	0.952	0.078	0.074
2.70	20.00	0.119	0.953	0.076	0.073
2.65	20.00	0.117	0.954	0.074	0.071
2.60	20.00	0.115	0.955	0.073	0.069
2.55	20.00	0.113	0.956	0.071	0.068
2.50	20.00	0.111	0.957	0.069	0.066
2.45	20.00	0.109	0.958	0.068	0.065
2.40	20.00	0.107	0.958	0.066	0.063
2.35	20.00	0.105	0.959	0.064	0.061
2.30	20.00	0.103	0.960	0.062	0.060
2.25	20.00	0.101	0.961	0.060	0.058
2.20	20.00	0.099	0.962	0.059	0.056
2.15	20.00	0.097	0.963	0.057	0.055
2.10	20.00	0.095	0.964	0.055	0.053
2.05	20.00	0.093	0.965	0.053	0.051
2.00	20.00	0.091	0.966	0.052	0.050
1.95	20.00	0.089	0.967	0.050	0.048
1.90	20.00	0.087	0.968	0.048	0.046
1.85	20.00	0.085	0.969	0.046	0.045
1.80	20.00	0.083	0.970	0.044	0.043
1.75	20.00	0.080	0.970	0.042	0.041
1.70	20.00	0.078	0.971	0.040	0.039
1.65	20.00	0.076	0.972	0.039	0.038
1.60	20.00	0.074	0.973	0.037	0.036
1.55	20.00	0.072	0.974	0.035	0.034
1.50	20.00	0.070	0.974	0.033	0.032
1.45	20.00	0.068	0.975	0.031	0.030
1.40	20.00	0.065	0.976	0.029	0.028
1.35	20.00	0.063	0.976	0.027	0.027
1.30	20.00	0.061	0.977	0.025	0.025
1.25	20.00	0.059	0.977	0.023	0.023
1.20	20.00	0.057	0.978	0.021	0.021
1.15	20.00	0.054	0.978	0.019	0.019
1.10	20.00	0.052	0.978	0.017	0.017
1.05	20.00	0.050	0.977	0.015	0.015
1.00	20.00	0.048	0.976	0.013	0.013
0.95	20.00	0.045	0.975	0.011	0.011
0.90	20.00	0.043	0.972	0.009	0.009
0.85	20.00	0.041	0.967	0.007	0.007
0.80	20.00	0.038	0.957	0.005	0.005
0.75	20.00	0.036	0.934	0.003	0.003
0.70	20.00	0.034	0.838	0.001	0.001
0.65	20.00	0.031	1.323	-0.001	-0.001
0.60	20.00	0.029	1.083	-0.003	-0.003
0.55	20.00	0.027	1.049	-0.005	-0.005
0.50	20.00	0.024	0.992	0.005	0.005
0.45	20.00	0.022	0.993	0.004	0.004
0.40	20.00	0.020	0.993	0.003	0.003
0.35	20.00	0.017	0.994	0.002	0.002
0.30	20.00	0.015	0.995	0.002	0.002
0.25	20.00	0.012	0.996	0.001	0.001
0.20	20.00	0.010	0.997	0.001	0.001
0.15	20.00	0.007	0.998	0.000	0.000
0.10	20.00	0.005	0.998	0.000	0.000
0.05	20.00	0.002	0.999	0.000	0.000

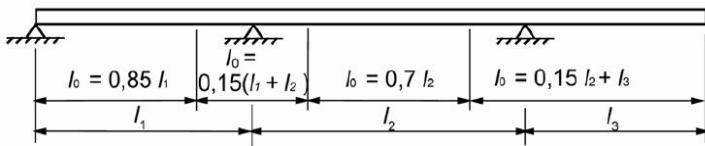
$$b_{\text{eff}} = \sum b_{\text{eff},i} + b_w \leq b$$

gde je:

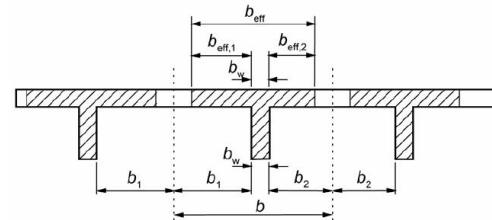
$$b_{\text{eff},i} = 0,2 b_i + 0,1 l_0 \leq 0,2 l_0$$

i

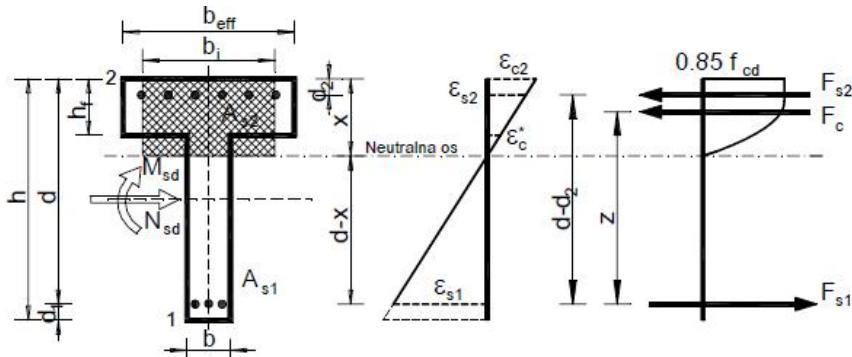
$$b_{\text{eff},i} \leq b_i$$



Slika 5.2: Definicija l_0 za proračun efektivne širine flanše



Slika 5.3: Parametri za efektivnu širinu flanše



h_f/d																			b_{eff}/b										
$\xi = X/d$																			λ_b										
0.550	0.525	0.500	0.475	0.450	0.425	0.400	0.375	0.350	0.325	0.300	0.275	0.250	0.225	0.200	0.175	0.150	0.125	0.100	0.075	0.050	0.025	1.5	2.0	2.5	3.0	3.5	4.0	4.5	5.0
0.550	0.525	0.500	0.475	0.450	0.425	0.400	0.375	0.350	0.325	0.300	0.275	0.250	0.225	0.200	0.175	0.150	0.125	0.100	0.075	0.050	0.025	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
0.550	0.513	0.489	0.464	0.437	0.413	0.386	0.362	0.335	0.309	0.284	0.259	0.232	0.207	0.181	0.155	0.130	0.103	0.078	0.052	0.026		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
0.550	0.513	0.487	0.461	0.436	0.409	0.383	0.357	0.330	0.303	0.276	0.249	0.221	0.194	0.166	0.139	0.111	0.083	0.056	0.028		0.99	0.99	0.99	0.99	0.99	0.99	0.99	0.99	
0.550	0.513	0.487	0.460	0.434	0.407	0.379	0.351	0.323	0.294	0.266	0.237	0.208	0.178	0.149	0.119	0.091	0.060	0.030	0.026		0.99	0.98	0.98	0.98	0.98	0.98	0.98	0.98	
0.550	0.512	0.485	0.459	0.431	0.403	0.374	0.345	0.315	0.285	0.254	0.223	0.192	0.160	0.129	0.097	0.065	0.032	0.026	0.026		0.98	0.97	0.97	0.97	0.96	0.96	0.96	0.96	
0.550	0.512	0.485	0.457	0.428	0.399	0.368	0.337	0.308	0.273	0.240	0.207	0.173	0.139	0.105	0.070	0.035	0.026	0.026	0.026		0.97	0.96	0.95	0.94	0.94	0.93	0.93	0.93	
0.550	0.511	0.483	0.454	0.425	0.394	0.362	0.329	0.295	0.260	0.224	0.188	0.151	0.114	0.076	0.038	0.026	0.026	0.026	0.026		0.96	0.94	0.93	0.92	0.91	0.91	0.91	0.90	
0.550	0.510	0.481	0.451	0.420	0.388	0.354	0.318	0.281	0.243	0.204	0.164	0.124	0.083	0.042	0.026	0.026	0.026	0.026	0.026		0.95	0.92	0.90	0.89	0.88	0.88	0.87	0.87	
0.550	0.509	0.479	0.448	0.415	0.381	0.344	0.305	0.265	0.228	0.180	0.136	0.091	0.046	0.026	0.026	0.026	0.026	0.026	0.026		0.93	0.90	0.87	0.86	0.85	0.84	0.84	0.83	
0.550	0.508	0.477	0.444	0.409	0.372	0.331	0.289	0.244	0.198	0.150	0.101	0.051	0.01	0.01	0.01	0.01	0.01	0.01	0.01		0.91	0.87	0.84	0.83	0.81	0.80	0.80	0.79	
0.550	0.507	0.473	0.433	0.401	0.360	0.316	0.268	0.218	0.166	0.112	0.056	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		0.90	0.84	0.81	0.79	0.78	0.76	0.76	0.75	
0.550	0.506	0.469	0.432	0.391	0.345	0.295	0.241	0.184	0.125	0.063	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		0.88	0.82	0.78	0.75	0.74	0.72	0.71	0.70	
0.550	0.502	0.464	0.423	0.378	0.326	0.268	0.206	0.140	0.071	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		0.86	0.79	0.74	0.72	0.70	0.68	0.67	0.66	
0.550	0.499	0.457	0.412	0.360	0.299	0.232	0.158	0.081	0.041	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		0.84	0.76	0.71	0.68	0.65	0.64	0.62	0.61	
0.550	0.494	0.448	0.397	0.335	0.268	0.181	0.093	0.026	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		0.82	0.73	0.68	0.64	0.61	0.59	0.58	0.57	
0.550	0.488	0.435	0.374	0.298	0.208	0.108	0.080	0.070	0.064	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		0.80	0.70	0.64	0.60	0.57	0.55	0.53	0.52	
0.550	0.479	0.418	0.342	0.243	0.127	0.078	0.067	0.060	0.058	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		0.78	0.67	0.60	0.56	0.53	0.51	0.49	0.48	
0.550	0.467	0.392	0.288	0.154	0.076	0.064	0.058	0.053	0.049	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		0.76	0.64	0.58	0.53	0.49	0.47	0.45	0.43	
0.550	0.449	0.347	0.192	0.074	0.062	0.054	0.049	0.045	0.042	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		0.74	0.66	0.50	0.45	0.41	0.38	0.36	0.34	
0.550	0.420	0.252	0.172	0.059	0.045	0.037	0.031	0.026	0.022	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		0.72	0.60	0.45	0.41	0.37	0.34	0.31	0.29	
0.550	0.381	0.171	0.056	0.047	0.041	0.037	0.031	0.026	0.022	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		0.70	0.69	0.53	0.43	0.37	0.33	0.29	0.27	

$$b_i = \left[1 - \frac{\alpha_v^*}{\alpha_v} \left(1 - \frac{h_f}{\xi \cdot d} \right) \cdot \left(1 - \frac{b}{b_{\text{eff}}} \right) \right] \cdot b_{\text{eff}} = \lambda_b \cdot b_{\text{eff}}$$

Tablice za odabir armature (grede)

Fi(mm)	kg/m	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
8	0,405	0,50	1,01	1,51	2,01	2,51	3,02	3,52	4,02	4,52	5,03	5,53	6,03	6,54	7,04	7,54
10	0,634	0,79	1,57	2,36	3,14	3,93	4,71	5,50	6,20	7,07	7,85	8,64	9,42	10,21	11,00	11,78
12	0,911	1,13	2,26	3,39	4,52	5,66	6,79	7,92	9,05	10,18	11,31	12,44	13,57	14,70	15,83	16,97
14	1,242	1,54	3,08	4,62	6,16	7,70	9,24	10,78	12,32	13,86	15,39	16,93	18,47	20,01	21,55	23,09
16	1,621	2,01	4,02	6,03	8,04	10,05	12,06	14,07	16,09	18,10	20,11	22,12	24,13	26,14	28,15	30,16
18	2,170	2,54	5,09	7,63	10,18	12,72	15,27	17,81	20,36	22,90	25,45	27,99	30,54	33,08	35,63	38,17
19	2,288	2,84	5,67	8,51	11,34	14,18	17,01	19,85	22,68	25,52	28,35	31,19	34,02	36,86	39,69	42,53
20	2,536	3,14	6,28	9,43	12,57	15,71	18,85	21,99	25,13	28,27	31,42	34,56	37,70	40,84	43,98	47,12
22	3,058	3,80	7,60	11,40	15,21	19,01	22,81	26,64	30,41	34,21	38,01	41,81	45,62	49,42	53,22	57,02
24	3,652	4,52	9,05	13,57	18,10	22,62	27,14	31,67	36,19	40,72	45,24	49,76	54,29	58,81	63,34	67,86
25	3,951	4,91	9,82	14,73	19,64	24,54	29,45	34,36	39,27	44,18	49,09	54,00	58,90	63,81	68,72	73,63
28	4,956	6,16	12,32	18,47	24,63	30,79	36,95	43,10	49,26	55,42	61,58	67,73	73,88	80,05	86,21	92,36
32	6,474	8,04	16,09	24,13	32,17	40,21	48,26	56,30	64,34	72,38	80,42	88,47	96,50	104,55	112,60	120,64
36	8,200	10,18	20,36	30,54	40,72	50,89	61,07	71,25	81,43	91,61	101,79	111,97	122,15	132,32	142,50	152,68
razmak armature/m	100,00	50,00	33,34	25,00	20,00	16,67	14,30	12,50	11,11	10,00	9,10	8,33	7,70	7,14	6,67	

Tip	Profili (mm)	Razmaci (mm)	Dimenziije (m)	kg/m2	kg/kom
R 131	5,0x4,2	150x250	6,00x2,20	1,50	19,80
R 131	5,0x4,6	150x250	6,00x2,20	1,63	21,50
R 139	4,2x4,2	100x250	6,00x2,20	1,55	20,50
R 166	4,6x4,2	100x250	6,00x2,20	1,76	23,30
R 166	4,6x4,6	100x250	6,00x2,20	1,85	24,50
R 188	6,0x4,2	150x250	6,00x2,20	1,96	26,00
R 188	6,0x4,6	150x250	6,00x2,20	2,08	27,50
R 196	5,0x4,2	150x250	6,00x2,20	2,00	26,50
R 226	6,0x4,2	125x250	6,00x2,20	2,27	30,00
R 257	7,0x5,0	150x250	6,00x2,20	2,72	35,80
R 283	6,0x4,6	100x250	6,00x2,20	2,77	36,60
R 283	6,0x5,0	100x250	6,00x2,20	2,88	38,00
R 335	8,0x5,0	150x250	6,00x2,20	3,33	44,00
R 335	8,0x6,0	150x250	6,00x2,20	3,63	48,00
R 385	7,0x5,0	100x250	6,00x2,20	3,68	48,60
R 424	9,0x6,0	150x250	6,00x2,20	4,34	57,30
R 503	8,0x5,0	100x200	6,00x2,20	4,77	63,00
R 503	8,0x5,0	100x250	6,00x2,20	4,58	60,50
R 503	8,0x6,0	100x250	6,00x2,20	4,89	64,60
R 524	10,0x6,0	150x250	6,00x2,15	5,15	68,00
R 636	9,0x6,0	100x250	6,00x2,15	5,95	78,50
R 785	10,0x6,0	100x250	6,00x2,15	7,35	97,00
R 785	10,0x6,0	100x200	6,00x2,20	7,39	97,50

Tip	Profili (mm)	Razmaci (mm)	Dimenziije (m)	kg/m2	kg/kom
Q 069	4,2x4,2	200x200	6,00x2,20	1,10	14,50
Q 131	5,0x5,0	150x150	6,00x2,20	2,12	28,00
Q 139	4,2x4,2	100x100	6,00x2,20	2,20	29,05
Q 166	4,6x4,6	100x100	6,00x2,20	2,64	34,90
Q 188	6,0x6,0	150x150	6,00x2,20	3,06	40,40
Q 196	5,0x5,0	100x100	6,00x2,15	3,07	40,50
Q 226	6,0x6,0	125x125	6,00x2,20	3,63	48,00
Q 257	7,0x7,0	150x150	6,00x2,20	4,16	55,00
Q 283	6,0x6,0	100x100	6,00x2,20	4,48	59,15
Q 335	8,0x8,0	150x150	6,00x2,20	5,45	72,00
Q 385	7,0x7,0	100x100	6,00x2,20	6,10	80,60
Q 424	9,0x9,0	150x150	6,00x2,20	6,81	90,00
Q 503	8,0x8,0	100x100	6,00x2,20	8,03	106,00
Q 524	10,0x10,0	150x150	6,00x2,20	8,40	110,90
Q 636	9,0x9,0	100x100	6,00x2,20	10,08	133,05
Q 785	10,0x10,0	100x100	6,00x2,20	12,46	164,50

Način opterećenja	Statička veličina	Način opterećenja u opterećenom polju								
		$x = (0.4 \div 0.5)L$	$\frac{P}{1/2}$	$\frac{P}{1/2}$	$\frac{P}{1/3} \frac{P}{1/3} \frac{P}{1/3}$	$\frac{P}{1/4} \frac{P}{1/2} \frac{P}{1/4}$	$\frac{P}{1/4} \frac{P}{1/4} \frac{P}{1/4}$	$\frac{P}{1/6} \frac{P}{1/3} \frac{P}{1/3} \frac{P}{1/6}$	$\frac{1/2}{1} \frac{1/2}{1}$	$\frac{0.41}{1} \frac{0.21}{1} \frac{0.41}{1}$
0.2001 0.2001	M ₁₁	0.070 pl ²	0.156 FI	0.222 FI	0.180 FI	0.258 FI	0.184 FI	0.095 KI	0.094 KI	0.089 KI
	M ₁₂	-	-	0.111 F	0.039 FI	0.266 FI	0.219 FI	-	-	-
	M ₁₃	-	-	-	-	0.023 FI	-0.080 FI	-	-	-
	M _{Bmin}	-0.125 pl ²	-0.188 FI	-0.333 FI	-0.281 FI	-0.469 FI	-0.396 FI	-0.156 KI	-0.155 KI	-0.151 KI
	R _A =Q _{1A}	0.375 pl	0.313 F	0.667 F	0.719 F	1.031 F	1.104 F	0.344 K	0.345 K	0.349 K
Za stalno opterećenje stavlja se G umjesto P, odnosno g. umjesto p.	R _{Bmax}	1.250 pl	1.375 F	2.667 F	2.563 F	3.938 F	3.792 F	1.312 K	1.310 K	1.302 K
	Q _{1Bmin}	-0.625 pl	-0.688 F	-1.333 F	-1.281 F	-1.969 F	-1.896 F	-0.656 K	-0.555' K	-0.651 K
	M _{11max}	0.096 pl ²	0.203 FI	0.278 FI	0.215 FI	0.316 FI	0.217 FI	0.129 KI	0.126 KI	0.121 KI
	M _{12max}	-	-	0.222 FI	0.145 FI	0.383 FL	0.318 FI	-	-	-
	M _{13max}	-	-	-	-	0.200 FI	0.085 FI	-	-	-
	M _B	-0.063 pl ²	-0.094 FI	-0.167 FI	-0.141 FI	-0.234 FI	-0.198 FI	-0.078 KI	-0.078 KI	-0.076 KI
	R _A =Q _{1Amax}	0.438 pl	0.406 F	0.833 F	0.859 F	1.266 F	1.302 F	0.422 K	0.422 K	0.424 K
	M _{11min}	-	-0.047 FI	-0.056 FI	-0.035 FI	-0.059 FI	-0.033 FI	-0.035 KI	-0.035 KI	-0.034 KI
	M _{12min}	-	-	-0.111 FI	-0.106 FI	-0.117 FI	-0.099 FI	-	-	-
	M _{13min}	-	-	-	-	-0.176 FI	-0.165 FI	-	-	-
	R _A =Q _{1Amin}	-0.063 pl	-0.094 F	-0.167 F	-0.141 F	-0.234 F	-0.198 F	-0.078 K	0.078 K	-0.076 K

Način opterećenja	Statička veličina	Način opterećenja u opterećenom polju								
		$x = (0.4 \div 0.5)L$	$\frac{P}{1/2}$	$\frac{P}{1/2}$	$\frac{P}{1/3} \frac{P}{1/3} \frac{P}{1/3}$	$\frac{P}{1/4} \frac{P}{1/2} \frac{P}{1/4}$	$\frac{P}{1/4} \frac{P}{1/4} \frac{P}{1/4}$	$\frac{P}{1/6} \frac{P}{1/3} \frac{P}{1/3} \frac{P}{1/6}$	$\frac{1/2}{1} \frac{1/2}{1}$	$\frac{0.41}{1} \frac{0.21}{1} \frac{0.41}{1}$
0.2105 1 0.20001	M ₁₁	0.080 pl ²	0.175 FI	0.244 FI	0.194 FI	0.281 FI	0.197 FI	0.108 KI	0.107 KI	0.102 KI
	M ₁₂	-	-	0.156 FI	0.081 FI	0.313 FI	0.258 FI	-	-	-
	M ₁₃	-	-	-	-	0.094 FI	-0.014 FI	-	-	-
	M ₂₁	0.025 pl ²	0.100 FI	0.067 FI	0.025 FI	0	-0.067 FI	0.042 KI	0.040 KI	0.063 KI
	M ₂₂	-	-	0.067 FI	0.025 FI	0.125 FI	0.100 FI	-	-	-
	M _B	-0.10C pl ²	-0.150 FI	-0.267 FI	-0.225 FI	-0.375 FI	-0.317 FI	-0.125 KI	-0.124 KI	-0.121 KI
	R _A =Q _{1A}	0.400 pl	0.350 F	0.733 F	0.775 F	1.125 F	1.183 F	0.375 K	0.376 K	0.379 K
	R _B	1.100 pl	1.150 F	2.267 F	2.225 F	3.375 F	3.317 F	1.125 K	1.124 K	1.121 K
	Q _{1B}	-0.600 pl	-0.650 F	-1.267 F	-1.225 F	-1.875 F	-1.817 F	-0.625 K	-0.624 K	-0.621 K
	Q _{2B} =-Q _{2C}	0.500 pl	0.500 F	1.000 F	1.000 F	1.500 F	1.500 F	0.500 K	0.500 K	0.500 K
	M _{11max}	0.101 pl ²	0.213 FI	0.289 FI	0.222 FI	0.328 FI	0.224 FI	0.136 KI	0.134 KI	0.128 KI
	M _{12max}	-	-	0.244 FI	0.166 FI	0.406 FI	0.338 FI	-	-	-
	M _{13max}	-	-	-	-	0.234 FI	0.118 FI	-	-	-
	M _{21 min}	-0.050 pl ²	-0.075 FI	-0.133 FI	-0.113 FI	-0.188 FI	-0.158 FI*	-0.063 KI	-0.062 KI	-0.061 KI
	M _{22 min}	-	-	-0.133 FI	-0.113 FI	-0.188 FI	-0.158 FI	-	-	-
	M _B	-0.050 pl ²	-0.075 FI	-0.133 FI	-0.113 FI	-0.188 FI	-0.158 FI	-0.063 KI	-0.062 KI	-0.061 KI
	R _A =Q _{1A} max	0.450 pl	0.425 F	0.867 F	0.888 F	1.313 F	1.342 F	0.375 K	0.376 K	0.379 K

Način opterećenja	Statička veličina	Način opterećenja u opterećenom polju								
		$x = (0.4 \div 0.5)L$	$\frac{P}{1/2}$	$\frac{P}{1/2}$	$\frac{P}{1/3} \frac{P}{1/3} \frac{P}{1/3}$	$\frac{P}{1/4} \frac{P}{1/2} \frac{P}{1/4}$	$\frac{P}{1/4} \frac{P}{1/4} \frac{P}{1/4}$	$\frac{P}{1/6} \frac{P}{1/3} \frac{P}{1/3} \frac{P}{1/6}$	$\frac{1/2}{1} \frac{1/2}{1}$	$\frac{0.41}{1} \frac{0.21}{1} \frac{0.41}{1}$
	M _{11min}	-0.025 pl ²	-0.038 FI	-0.044 FI	-0.028 FI	-0.047 FI	-0.026 FI	-0.028 KI	-0.028 KI	-0.027 KI
	M _{12 min}	-	-	-0.089 FI	-0.084 FI	-0.094 FI	-0.079 FI	-	-	-
	M _{13 min}	-	-	-	-	-0.141 FI	-0.132 FI	-	-	-
	M _{21 max}	0.075 pl ²	0.175 FI	0.200 FI	0.138 FI	0.188 FI	(0.100 FI)	0.104 KI	0.102 KI	0.096 KI
	M _{22 max}	-	-	0.200 FI	0.138 FI	0.313 FI	0.258 FI	-	-	-
	M _B	-0.050 pl ²	-0.075 FI	-0.133 FI	-0.113 FI	-0.188 FI	-0.158 FI	-0.063 KI	-0.062 KI	-0.061 KI
	R _A =Q _{1A} min	-0.050 pl	-0.075 F	-0.133 F	-0.113 F	-0.188 F	-0.158 F	-0.063 K	-0.062 K	-0.061 K
	M _{B min}	-0.117 pl ²	-0.175 FI	-0.311 FI	-0.263 FI	-0.438 FI	-0.369 FI	-0.146 KI	-0.145 KI	-0.142 KI
	M _C	-0.033 pl ²	-0.050 FI	-0.089 FI	-0.075 FI	-0.125 FI	-0.106 FI	-0.041 KI	-0.041 KI	-0.041 KI
	R _{B max}	1.200 pl	1.300 F	2.533 F	2.450 F	3.750 F	3.633 F	1.251 K	1.249 K	1.244 K
	Q _{1B min}	-0.617 pl	-0.675 F	-1.311 F	-1.263 F	-1.937 F	-1.869 F	-0.646 K	-0.645 K	-0.642 K
	Q _{2B max}	0.583 pl	0.625 F	1.222 F	1.188 F	1.813 F	1.764 F	0.605 K	0.604 K	0.602 K
	M _{B max}	0.017 pl ²	0.025 FI	0.044 FI	0.038 FI	0.063 FI	0.053 FI	0.022 KI	0.021 KI	0.021 KI
	M _C	-0.067 pl ²	-0.100 FI	-0.178 FI	-0.150 FI	-0.250 FI	-0.211 FI	-0.083 KI	-0.083 KI	-0.081 KI
	Q _{1B max}	0.017 pl	0.025 F	0.044 F	0.038 F	0.063 F	0.053 F	0.022 K	0.021 K	0.021 K
	Q _{2B min}	-0.083 pl	-0.125 F	-0.222 F	-0.188 F	-0.313 F	-0.264 F	-0.105 K	-0.104 K	-0.102 K